

Virtual plane-wave imaging via Marchenko redatuming

Giovanni Angelo Meles, Kees Wapenaar and Jan Thorbecke

Department of Geoscience and Engineering, Delft University of Technology, Stevinweg 1, 2628 CN Delft, The Netherlands. E-mail: G.A.Meles@tudelft.nl

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SUMMARY

Marchenko redatuming is a novel scheme used to retrieve up- and downgoing Green's functions in an unknown medium. Marchenko equations are based on reciprocity theorems and are derived on the assumption of the existence of functions exhibiting space–time focusing properties once injected in the subsurface. In contrast to interferometry but similarly to standard migration methods, Marchenko redatuming only requires an estimate of the direct wave from the virtual source (or to the virtual receiver), illumination from only one side of the medium and no physical sources (or receivers) inside the medium. In this contribution we consider a different time-focusing condition within the frame of Marchenko redatuming that leads to the retrieval of virtual plane-wave responses. As a result, it allows multiple-free imaging using only a 1-D sampling of the targeted model at a fraction of the computational cost of standard Marchenko schemes. The potential of the new method is demonstrated on 2-D synthetic models.

Key words: Controlled source seismology; Seismic interferometry; Wave scattering and diffraction.

1 INTRODUCTION

Marchenko redatuming estimates Green's functions between the earth's surface and arbitrary locations in the subsurface. Differently from seismic interferometry, in Marchenko redatuming no real sources, nor receivers, are required at the chosen subsurface locations (Broggini *et al.* 2012b; Wapenaar *et al.* 2014). These Green's functions are evaluated using reciprocity theorems involving the so-called 'focusing functions', that is, wavefields which achieve space–time focusing in the subsurface.

In principle, redatumed Green's functions can be used to provide multiple-free images directly (Behura *et al.* 2014; Broggini *et al.* 2014). However, this approach requires as many virtual sources as there are image points in the subsurface. Marchenko redatuming also allows one to perform redatuming of the reflection response from the surface to a finite number of depth levels and to apply standard imaging in between those datum levels (Wapenaar *et al.* 2014; Ravasi *et al.* 2016). In that case, however, the redatumed reflection responses still include internal multiples reverberating below the redatuming level, which again may diminish the quality of resulting images if the distance between the redatuming levels is too large.

Other applications of the Marchenko method include demultiple schemes (Meles *et al.* 2015, 2016; van der Neut & Wapenaar 2016; da Costa Filho *et al.* 2017b), microseismic source localization (Behura *et al.* 2013; van der Neut *et al.* 2017), inversion (van der Neut & Fokkema 2018) and homogeneous Green's functions retrieval (Urruticoechea & Wapenaar 2017; Wapenaar *et al.* 2018).

Despite its requirements on the quality of the reflection response (e.g. knowledge and accurate deconvolution of the source wavelet, co-location of sources and receiver and knowledge of the absolute scaling factor of the recorded data), the Marchenko scheme has already been successfully applied to field data (van der Neut *et al.* 2015b; Ravasi *et al.* 2016; da Costa Filho *et al.* 2017a; Jia *et al.* 2017; Staring *et al.* 2017). Moreover, recent advances have shown how the requirements above can be considerably relaxed by combining the Marchenko equations with a one-way version of the Rayleigh integral representation (Ravasi 2017).

In this contribution we show how focusing functions associated with virtual plane-wave responses can be derived by imposing a time-focusing condition in the subsurface, which allows the derivation of a new set of Marchenko equations. The virtual plane-wave responses can be used to efficiently image the subsurface involving only a fraction of virtual responses as compared to standard Marchenko methods. The proposed method thus stands as an ideal bridge between areal-source methods for primaries (Rietveld *et al.* 1992) and the extended virtual-source Marchenko method addressed by Broggini *et al.* (2012a).

Potential and limitations of the new strategy are illustrated by means of numerical examples.

2 METHOD AND THEORY

In this section we briefly introduce reciprocity theorems and use them to derive the coupled Marchenko equations. To simplify our derivations, we will make use of both time and frequency domain

expressions. Following standard formalism, we will indicate wavefields in the time and frequency domain as $p(\mathbf{x}, z, t)$ and $\hat{p}(\mathbf{x}, z, \omega)$, respectively.

Reciprocity theorems for one-way flux-normalized wavefields relate up- and downgoing wavefield components of two states A and B evaluated at two depths. Convolution and cross-correlation reciprocity theorems can be expressed in the frequency domain as follows (Wapenaar & Grimbergen (1996)):

$$\int_{\Lambda_a} d^2\mathbf{x} \{\hat{p}_A^+ \hat{p}_B^- - \hat{p}_A^- \hat{p}_B^+\} = \int_{\Lambda_f} d^2\mathbf{x} \{\hat{p}_A^+ \hat{p}_B^- - \hat{p}_A^- \hat{p}_B^+\}, \quad (1)$$

$$\int_{\Lambda_a} d^2\mathbf{x} \{\hat{p}_A^+ \hat{p}_B^{+*} - \hat{p}_A^- \hat{p}_B^{-*}\} = \int_{\Lambda_f} d^2\mathbf{x} \{\hat{p}_A^+ \hat{p}_B^{+*} - \hat{p}_A^- \hat{p}_B^{-*}\}, \quad (2)$$

where $*$ is complex conjugation, subscripts A and B relate to the corresponding states, superscripts $+$ and $-$ indicate down- and upgoing constituents, and Λ_a and Λ_f stand for two arbitrary depth levels.

Eqs (1) and (2) assume that the medium parameters are identical for both states in the volume circumscribed by Λ_a and Λ_f , and that no sources exist between these depth levels. Moreover, while eq. (1) is valid for lossy media, eq. (2) requires the medium to be lossless between the levels Λ_a and Λ_f , thus posing a limitation to the methodology presented here (for an extension to account for dissipation see Slob (2016)). Moreover, evanescent waves are neglected in eq. (2).

We will consider Λ_a and Λ_f to be the acquisition surface and a redatuming level, respectively. Moreover, we consider for state A a truncated medium identical to the physical medium above Λ_f and reflection-free below this level, while for state B we choose the physical medium.

We now discuss and define the properties of the wavefield for state A for two different focusing conditions, which we will refer to as f and F .

In standard space-time focusing, it is assumed that the downgoing component of the focusing function representing state A, that is, f_1^+ , satisfies the following focusing condition along Λ_f : $f_1^+(\mathbf{x}, z_f; \mathbf{x}_F, z_f; t) = \delta(t)\delta(\mathbf{x} - \mathbf{x}_F)$, where \mathbf{x}_F, z_f are the coordinates of a focal point in the subsurface (in the frequency domain this becomes: $\forall \omega, \hat{f}_1^+(\mathbf{x}, z_f; \mathbf{x}_F, z_f; \omega) = \delta(\mathbf{x} - \mathbf{x}_F)$). Moreover, since it is assumed that the medium in state A is truncated below Λ_f , no upgoing component f_1^- exists along this lower boundary regardless of its properties along Λ_a (Fig. 1a).

For state B, following the standard approach, we place a point source for a downgoing wavefield at \mathbf{x}_B at depth z_a just above the surface, so that along Λ_a we have $\hat{p}_B^+ = \delta(\mathbf{x} - \mathbf{x}_B)$ and $\hat{p}_B^- = \hat{R}(\mathbf{x}, z_a; \mathbf{x}_B, z_a; \omega)$, where \hat{R} indicates the reflection response of the physical medium at the surface, and on Λ_f we have $p_B^{+/-} = g^{+/-}(\mathbf{x}, z_f; \mathbf{x}_B, z_a; \omega)$, where g^+ and g^- are the down- and upgoing parts of the Green's function.

Substituting these definitions into eqs (1) and (2) we get:

$$\begin{aligned} \hat{f}_1^-(\mathbf{x}_B, z_a; \mathbf{x}_F, z_f; \omega) + \hat{g}^-(\mathbf{x}_F, z_f; \mathbf{x}_B, z_a; \omega) &= \\ \int_{\Lambda_a} d^2\mathbf{x} \hat{R}(\mathbf{x}, z_a; \mathbf{x}_B, z_a; \omega) \hat{f}_1^+(\mathbf{x}, z_a; \mathbf{x}_F, z_f; \omega), \\ \hat{f}_1^+(\mathbf{x}_B, z_a; \mathbf{x}_F, z_f; \omega) - \hat{g}^{+*}(\mathbf{x}_F, z_f; \mathbf{x}_B, z_a; \omega) &= \\ \int_{\Lambda_a} d^2\mathbf{x} \hat{R}^*(\mathbf{x}, z_a; \mathbf{x}_B, z_a; \omega) \hat{f}_1^-(\mathbf{x}, z_a; \mathbf{x}_F, z_f; \omega), \end{aligned} \quad (3)$$

or, using the compact, time-domain formalism introduced in van der Neut *et al.* (2015a):

$$\begin{aligned} \mathbf{f}_1^- + \mathbf{g}^- &= \mathbf{R}\mathbf{f}_1^+, \\ \mathbf{f}_1^+ - \mathbf{g}^{+*} &= \mathbf{R}^*\mathbf{f}_1^-, \end{aligned} \quad (4)$$

where the superscript $*$ indicates time reversal.

We now analyse this standard problem in more detail and show how the algorithm that provides its solution can be easily extended to problems involving different focusing conditions. The underdetermined system in eq. (4), which represents the basis for standard Marchenko redatuming, can be additionally simplified invoking a separation operator Θ_f to annihilate the Green's function terms:

$$\begin{aligned} \Theta_f \mathbf{f}_1^- &= \Theta_f \mathbf{R}\mathbf{f}_1^+, \\ \Theta_f \mathbf{f}_1^+ &= \Theta_f \mathbf{R}^* \mathbf{f}_1^-. \end{aligned} \quad (5)$$

This leads, after decomposing the focusing function into a direct and a coda component (i.e. setting $\mathbf{f}_1^+ = \mathbf{f}_{1d}^+ + \mathbf{f}_{1m}^+$, and using $\Theta_f \mathbf{f}_1^- = \mathbf{f}_1^-$ and $\Theta_f \mathbf{f}_1^+ = \mathbf{f}_{1m}^+$), to the linear problem

$$[\mathbf{I} - \Theta_f \mathbf{R}^* \Theta_f \mathbf{R}] \mathbf{f}_{1m}^+ = \Theta_f \mathbf{R}^* \Theta_f \mathbf{R} \mathbf{f}_{1d}^+, \quad (6)$$

which, under standard convergence conditions (Fokkema & van den Berg 2013), is solved by

$$\mathbf{f}_{1m}^+ = \sum_{k=0}^{\infty} (\Theta_f \mathbf{R}^* \Theta_f \mathbf{R})^k \mathbf{f}_{1d}^+. \quad (7)$$

Once the focusing functions are found, they are inserted in eq. (4), yielding the point-source Green's functions \mathbf{g}^- and \mathbf{g}^+ .

More details about the derivation of this series solution can be found in van der Neut *et al.* (2015a), while in Dukalski & de Vos (2017) other algorithms to solve eq. (6) are analysed.

We now consider a different focusing condition, which we will refer to as 'time-focusing condition' and show how its imposition results in the same Marchenko equations discussed above. For the time-focusing approach we refer to the focusing wavefield in state A as F_1 . We assume F_1 to be defined in a medium truncated below Λ_f , and therefore also in this case no upgoing component F_1^- exists along this lower boundary regardless of its properties along Λ_a . However, differently from the standard space-time focusing approach, we define F_1^+ as satisfying the following time-focusing condition along Λ_f : $\forall \mathbf{x} \in \Lambda_f, F_1^+(\mathbf{x}, z_f; z_f; t) = \delta(t)$, where z_f is the depth of the horizontal focal plane in the subsurface.

Note that in the frequency domain this becomes $\forall \mathbf{x} \in \Lambda_f, \forall \omega, \hat{F}_1^+(\mathbf{x}, z_f; z_f; \omega) = 1$. Note also that the time-focusing condition can be interpreted as a spatial integral along Λ_f of space-time focusing conditions, namely,

$$F_1^+(\mathbf{x}, z_f; z_f; t) = \int_{\Lambda_f} d^2\mathbf{x}_F f_1^+(\mathbf{x}, z_f; \mathbf{x}_F, z_f; t). \quad (8)$$

It is therefore clear that the focusing function F_1 could be obtained by integrating an appropriate set of focusing functions f_1 , each involving the solution of a Marchenko equation (see eq. 7). We will show in the following that the solution of a single Marchenko equation can provide the same result.

For state B we consider again a point source for a downgoing wavefield at \mathbf{x}_B just above the surface.

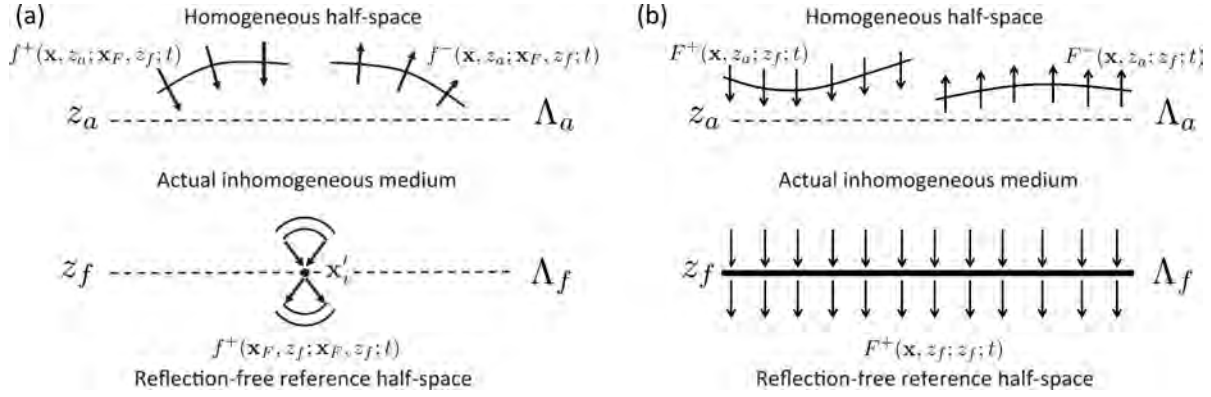


Figure 1. Down- and upgoing components of the focusing functions of the 3-D wave equation in a reference configuration. (a) Standard space-time focusing function f_1 , leading to point-source responses (Green's functions). (b) Time focusing function F_1 , leading to areal-source responses.

Substituting these definitions into eqs (1) and (2) we get:

$$\begin{aligned} \hat{F}_1^-(\mathbf{x}_B, z_a; z_f; \omega) + \hat{G}^-(z_f; \mathbf{x}_B, z_a; \omega) &= \\ \int_{\Lambda_a} d^2\mathbf{x} \hat{R}(\mathbf{x}, z_a; \mathbf{x}_B, z_a; \omega) \hat{F}_1^+(\mathbf{x}, z_a; z_f; \omega), \\ \hat{F}_1^+(\mathbf{x}_B, z_a; z_f; \omega) - \hat{G}^{+*}(z_f; \mathbf{x}_B, z_a; \omega) &= \\ \int_{\Lambda_a} d^2\mathbf{x} \hat{R}^*(\mathbf{x}, z_a; \mathbf{x}_B, z_a; \omega) \hat{F}_1^-(\mathbf{x}, z_a; z_f; \omega), \end{aligned} \quad (9)$$

where

$$\begin{aligned} \hat{G}^-(z_f; \mathbf{x}_B, z_a; \omega) &= \int_{\Lambda_f} d^2\mathbf{x} \hat{g}^-(\mathbf{x}, z_f; \mathbf{x}_B, z_a; \omega), \\ \hat{G}^+(z_f; \mathbf{x}_B, z_a; \omega) &= \int_{\Lambda_f} d^2\mathbf{x} \hat{g}^+(\mathbf{x}, z_f; \mathbf{x}_B, z_a; \omega), \end{aligned} \quad (10)$$

or, using again the compact, time-domain formalism:

$$\begin{aligned} \mathbf{F}_1^- + \mathbf{G}^- &= \mathbf{R}\mathbf{F}_1^+, \\ \mathbf{F}_1^+ - \mathbf{G}^{+*} &= \mathbf{R}^*\mathbf{F}_1^-. \end{aligned} \quad (11)$$

Similarly to what considered in eq. (4), the set of equations in eq. (11) is also underdetermined. As discussed above, the key ingredient to solve the system in eq. (4) is the existence of an appropriate separation operator.

Such an operator does not necessarily exist only for the space-time focusing system (4), as already preliminarily observed in Brogini *et al.* (2012a) for slightly spatially extended virtual sources. Here we generalize the observation of Brogini *et al.* (2012a), now considering plane-wave spatially extended sources. More precisely, we postulate that when a focusing function \mathbf{F}_1^+ satisfies the time-focusing property discussed above, a separation operator Θ_F (based on the first arrival of the response of $\int_{\Lambda_f} d^2\mathbf{x} g^+(\mathbf{x}, z_f; t; \mathbf{x}', z_a; 0)$, which can be interpreted as a plane-wave source based on reciprocity) can be successfully applied to eq. (11).

In this scenario, the existence of a separation operator reduces (11) into:

$$\begin{aligned} \Theta_F \mathbf{F}_1^- &= \Theta_F \mathbf{R} \mathbf{F}_1^+, \\ \Theta_F \mathbf{F}_1^+ &= \Theta_F \mathbf{R}^* \mathbf{F}_1^-. \end{aligned} \quad (12)$$

Following again the decomposition into a direct and coda component of the downgoing focusing function, this leads to the solution for the focusing function:

$$\mathbf{F}_1^+ = \sum_{k=0}^{\infty} (\Theta_F \mathbf{R}^* \Theta_F \mathbf{R})^k \mathbf{F}_{1d}^+. \quad (13)$$

Once the focusing functions are found, they are inserted in eq. (11), yielding the plane-wave source Green's functions $\hat{G}^-(z_f; \mathbf{x}_B, z_a; \omega)$ and $\hat{G}^{+*}(z_f; \mathbf{x}_B, z_a; \omega)$. This scheme therefore results in the retrieval of plane-wave up- and downgoing areal-receiver responses (by invoking reciprocity, these responses can be related to the down- and uppropagating areal-source responses discussed in Rietveld *et al.* 1992) rather than standard up- and downgoing Green's functions as in van der Neut *et al.* (2015a).

Once these plane-wave responses are available, they could be used within the areal-source framework (Rietveld *et al.* 1992).

3 NUMERICAL EXAMPLES

3.1 Focusing performances

We illustrate the potential of the iterative solutions algorithm for areal-source responses with finite-difference examples (Thorbecke *et al.* 2017). We consider the 2-D inhomogeneous subsurface model in Fig. 2.

First we assess the focusing performances of the solution of eq. (7) when a separation operator Θ_F and an initial focusing function \mathbf{F}_{1d}^+ associated with the first arrival of $\int_{\Lambda_f} d^2\mathbf{x} g^+(\mathbf{x}, z_f; t; \mathbf{x}', z_a; 0)$ are used.

We consider two arbitrarily chosen different depth levels (Lines '1' and '2' in Fig. 2). We then solve eq. (13) for initial focusing functions \mathbf{F}_{1d}^+ related to the depth levels of Lines '1' and '2', respectively, computing these direct components using the smooth models in Figs 2(c) and (d). The resulting up- and downgoing focusing functions are shown in Fig. 3. We then inject the retrieved downgoing focusing functions \mathbf{F}_1^+ (Figs 3a and c) into the corresponding truncated media, and record their response along Lines '1' and '2', respectively.

Fig. 4 shows that for both cases the focusing is very good, with only small amplitude artefacts contaminating the wavefield along the focal plane (red arrows in Fig. 4). Note that Line '1' crosses an interface, and therefore represents a particularly challenging problem due to the intrinsic limitations of the Marchenko method at interfaces, where the validity of the separation operator can be violated (Vasconcelos *et al.* 2014). The overall focusing performances are comparable to those of the standard Marchenko method, shown in Fig. 5 for representative points located close to or far-away from interfaces (Figs 2a–d), where artefacts (partially due to the finite acquisition aperture) are also seen to contaminate the focusing (red arrows in Fig. 5). Note that smooth models (see Figs 2c and d) were

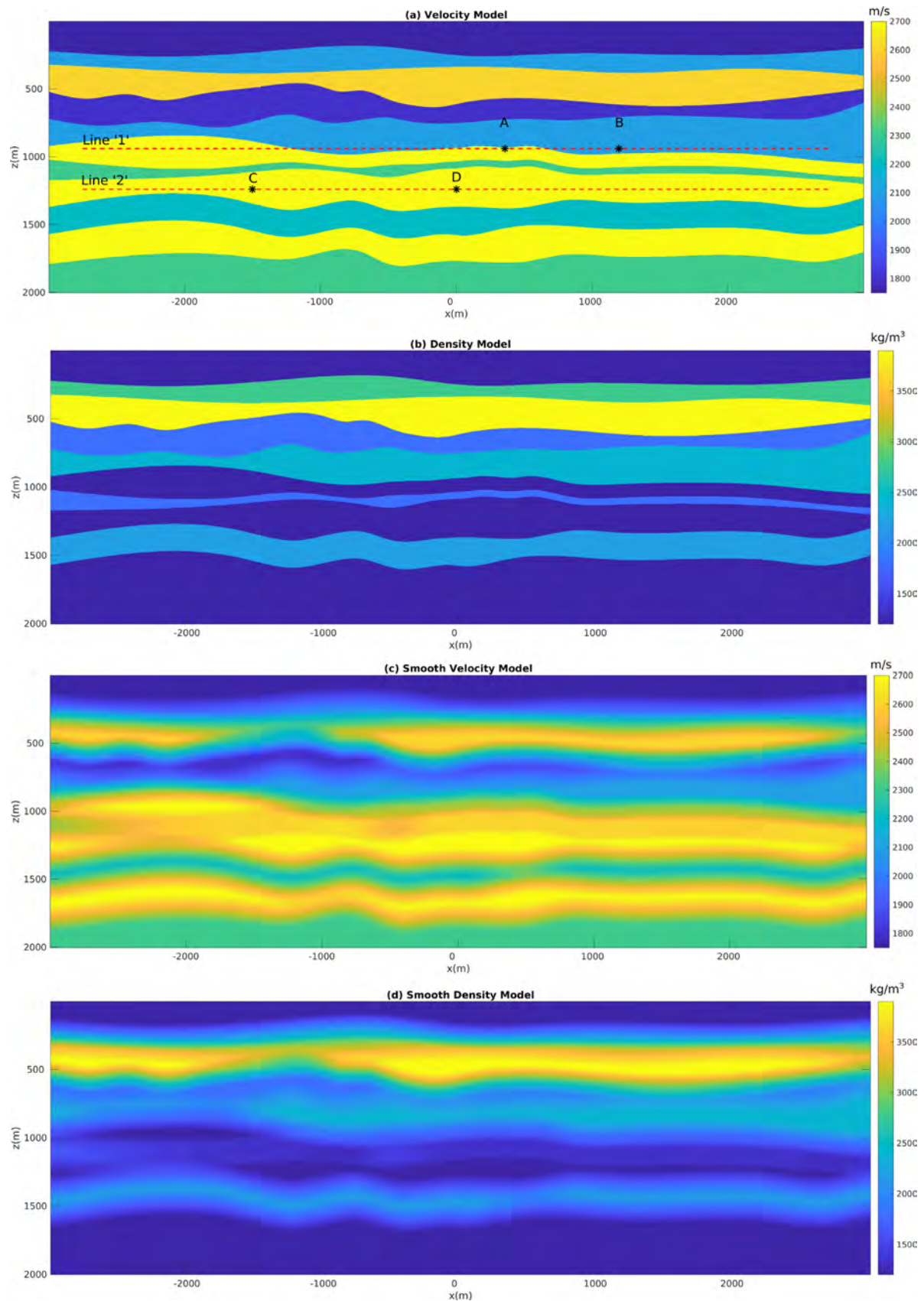


Figure 2. (a) Velocity model used in the first numerical experiment. Dashed lines and stars represent subsurface planes and points for time and space-time focusing, respectively. (b) Density model used in the numerical experiment. (c and d) Smooth velocity and density models used to provide input for Marchenko redatuming.

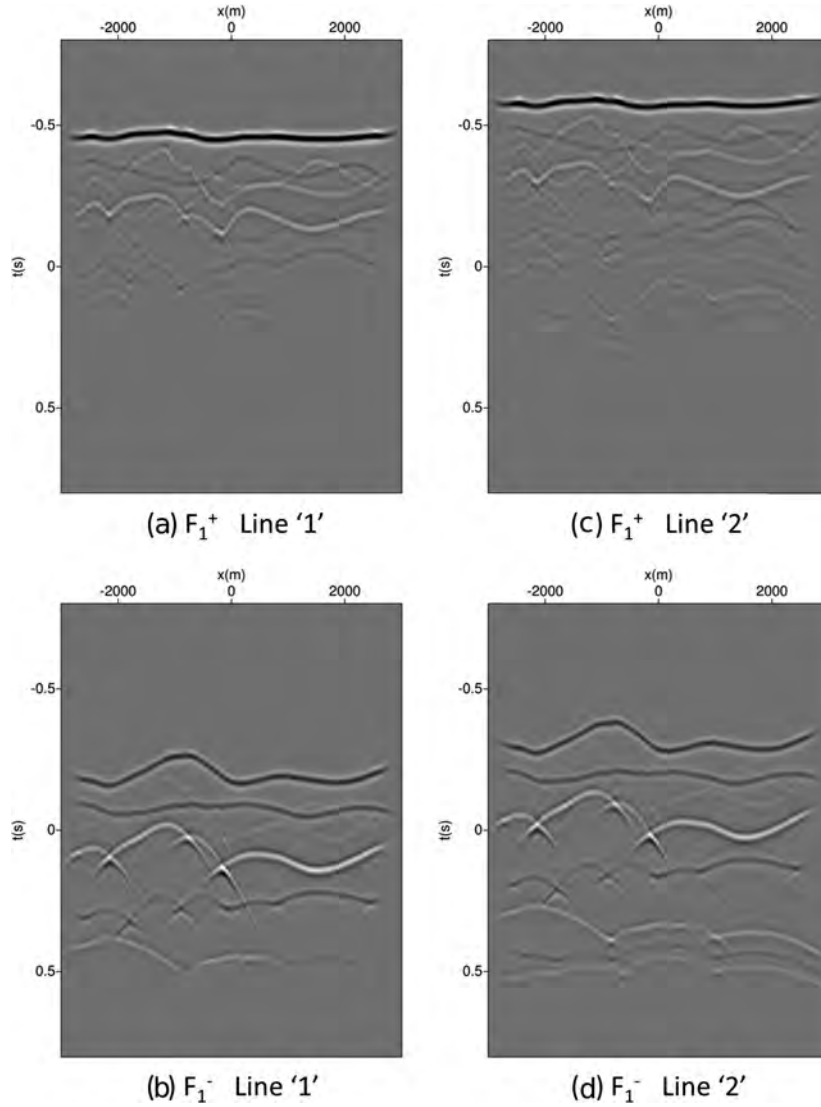


Figure 3. (a) Downgoing component of the focusing function F_1 associated with F_{1d+} being first arrival of $\int_{L_1} d^2 \mathbf{x} g^+(\mathbf{x}, z_f; t; \mathbf{x}', z_a; 0)$. (b) Upgoing component of the focusing function F_1 associated with F_{1d+} being the first arrival of $\int_{L_1} d^2 \mathbf{x} g^+(\mathbf{x}, z_f; t; \mathbf{x}', z_a; 0)$. (c and d) As for panels (a) and (b), but for F_{1d+} associated with the first arrival of $\int_{L_2} d^2 \mathbf{x} g^+(\mathbf{x}, z_f; t; \mathbf{x}', z_a; 0)$.

used to initiate the focusing process, and that perfect foci cannot be expected.

Fig. 6 compares directly modelled and retrieved Marchenko areal-source responses at the surface for Lines ‘1’ and ‘2’, respectively. As a direct consequence of the excellent focusing performances demonstrated in Fig. 4, the match between the modelled and the retrieved areal responses is also very good, with mainly tapering-related minor differences in the left- and right-most portions of the gather.

3.2 Imaging results

As mentioned in the introduction, redatumed Green’s functions can be used to provide multiple-free images directly, by cross-correlation of upgoing and direct downgoing wavefields in the subsurface (Behura *et al.* 2014). However, this approach is expensive, as it requires as many virtual sources as there are image points in the subsurface (number of required Marchenko solutions: $nx \times nz$

in 2-D, or $nx \times ny \times nz$ in 3-D, where nx , ny and nz stand for the number of image points along the x , y and z axes, respectively).

With Marchenko areal-source responses, however, we can use a single redatumed solution to image a whole line/plane at once (number of required Marchenko solutions: nz in 2-D as well as in 3-D). To achieve this, we use the following redatumed reflectivity and standard migration imaging condition definitions, in the frequency domain:

$$\begin{aligned} \hat{R}(\mathbf{x}, z_f; \omega) &= \int_{\Lambda_a} d^2 \mathbf{x}' \hat{g}_d^{+*}(\mathbf{x}, z_f; \mathbf{x}', z_a; \omega) \hat{G}^-(z_f; \mathbf{x}', z_a; \omega), \\ I(\mathbf{x}, z_f) &= \int_{\mathbb{R}} d\omega \hat{R}(\mathbf{x}, z_f; \omega). \end{aligned} \quad (14)$$

Note that the imaging condition in eq. (14) can be seen as an integral along the focal plane of point-source imaging conditions (this integration is implicit in \hat{G}^-). We expect this integration to reduce the lateral resolution of the final image due to poorer angle-illumination. In the following we will present a strategy to account for this limitation.

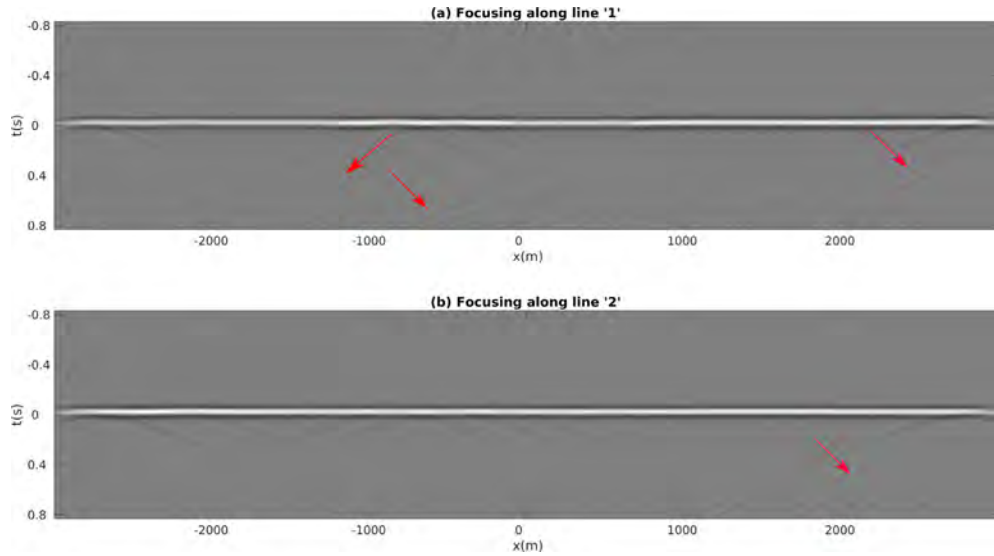


Figure 4. (a) Time-focusing along Line '1' in Fig. 2(a). (b) Time-focusing along Line '2' in Fig. 2(a). Red arrows point at small-amplitude artefacts.

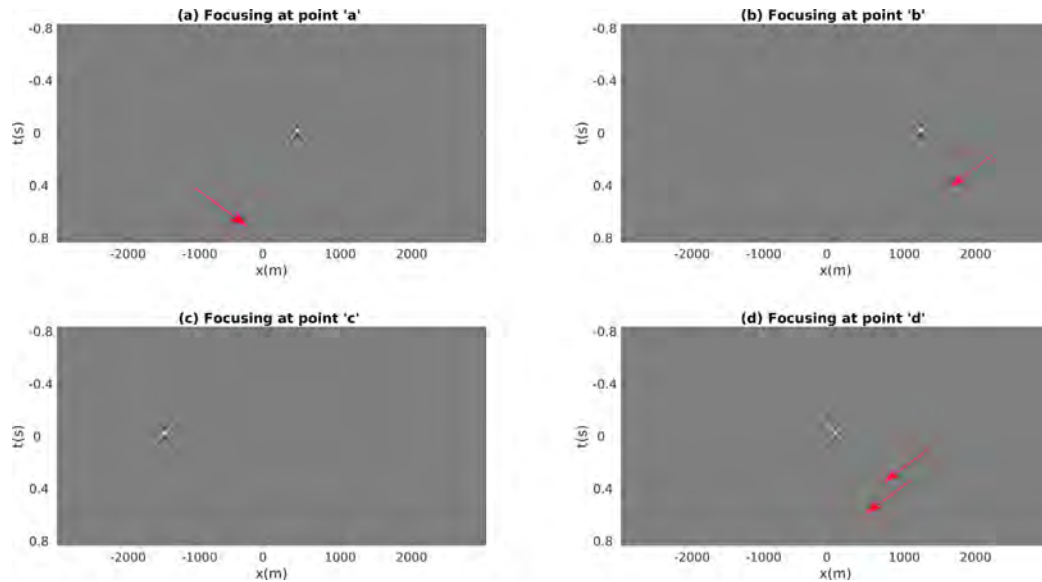


Figure 5. (a) Space-time focusing at point 'a' in Fig. 2. (b–d) As for (a), but for points (b)–(d) in Fig. 2. Red arrows point at small-amplitude artefacts.

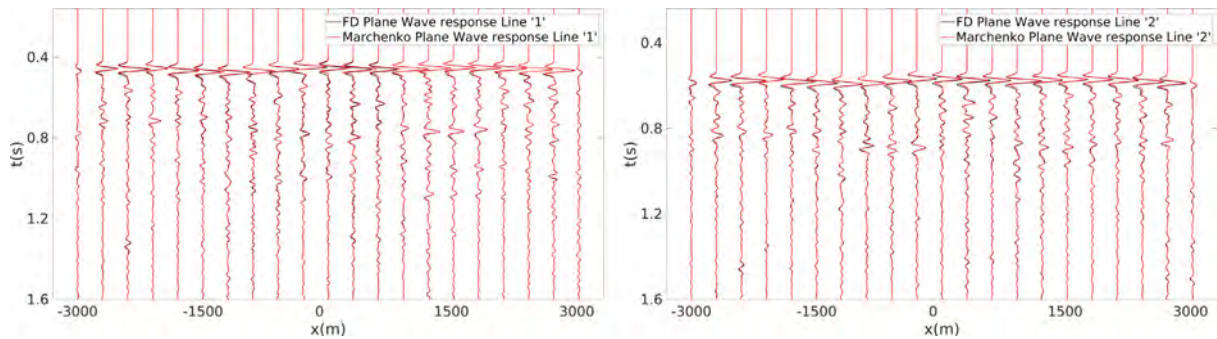


Figure 6. (a) FD modelled (black lines) and Marchenko (red lines) areal-source responses for Line '1'. (b) As for (a), but for Line '2'.

We apply our new imaging condition to the model discussed in the previous section. In this case we sample in depth every 5 m, and consequently to image the entire domain we employ 400 virtual areal sources. Note that imaging the whole model at a 5

m sampling rate using other Marchenko schemes would involve the computation and migration of up to 400×1200 virtual point-source responses, which would require considerable CPU or RAM resources. An exhaustive analysis about the computational burden

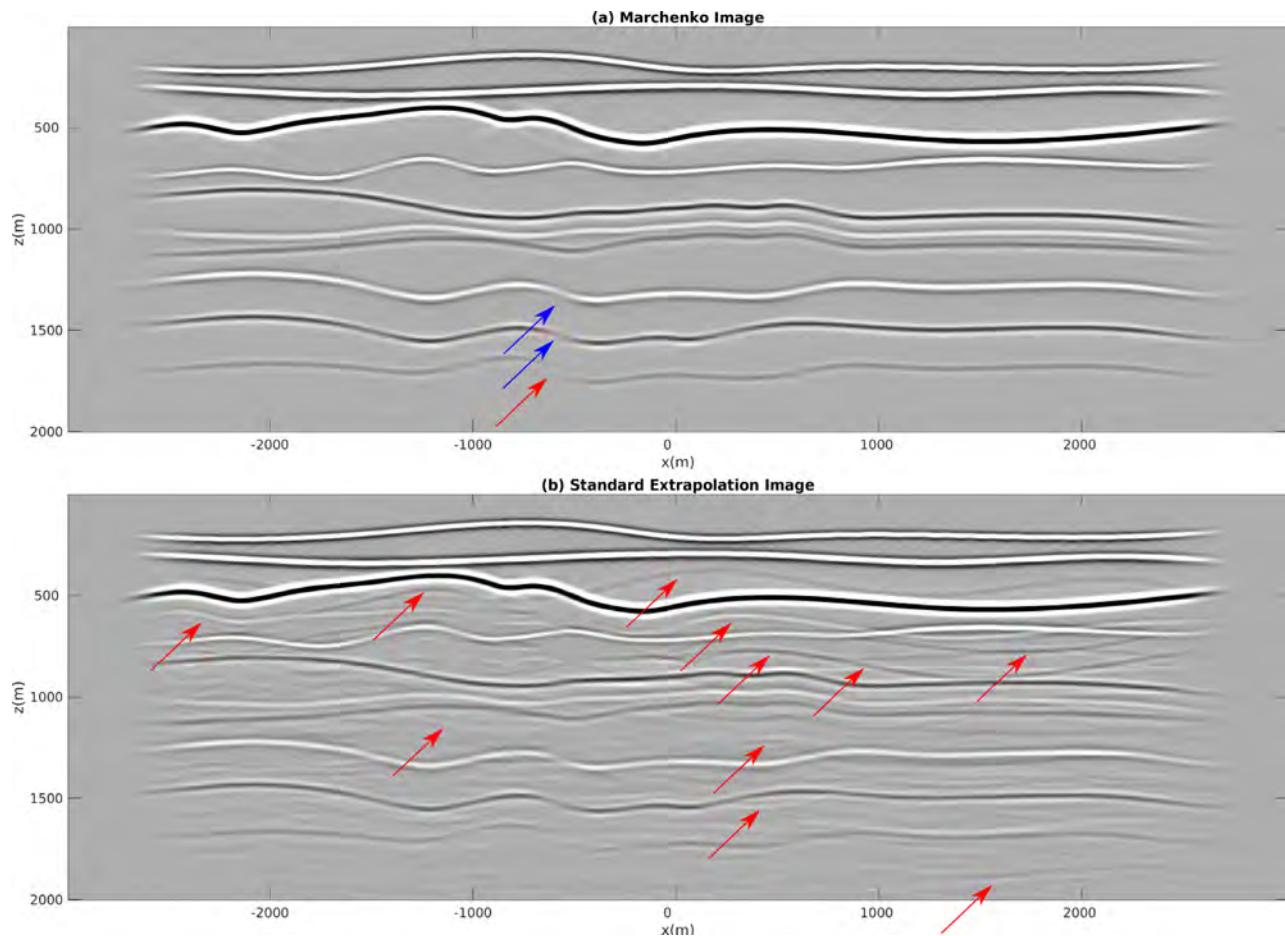


Figure 7. (a) Migration result using the imaging condition of eq. (14) and Marchenko redatumed virtual-plane wavefields. The red arrow points at a poorly imaged dipping layer, whereas the blue arrows point at similar structures that are properly imaged. (b) Migration result using standard one-way extrapolation of virtual-plane wavefields. Red arrows point at multiple-related artefacts.

of the Marchenko method as an imaging tool can be found in Behura *et al.* (2014). The migration associated with the imaging condition in eq. (14) is shown in Fig. 7(a). Each interface is properly imaged, while no multiple-related artefacts are present. Only a dipping layer in the bottom of the model is relatively poorly imaged (red arrow in Fig. 7a), partially due to its smaller impedance contrast. In any case, other structures with similar geometry are properly imaged (blue arrows in Fig. 7a). Multiple-related artefacts, on the other hand, contaminate the image if we migrate the upgoing response associated with the same areal sources obtained through standard one-way wavefield extrapolation (Fig. 7b). Note that in the migration step the same smooth models depicted in Figs 2(c) and (d) employed for Marchenko redatuming were used.

We further investigate the potential and limitations of the Marchenko plane-wave imaging scheme by considering a more complex subsurface model (Figs 8a and b). Differently from the medium of the first experiment (Fig. 2), the model considered here comprises dipping structures and diffractors. We follow the same imaging strategy discussed for the first numerical experiment, that is, we initially compute Marchenko areal-source responses for a set of evenly spaced (sampling every 5 m in depth) horizontal boundaries and we then apply the redatuming and imaging condition discussed in eq. (14). As for the previous experiment, we employ smooth velocity and density distributions both for the Marchenko and migration steps (Figs 8c and d).

The migration associated with the imaging condition in eq. (14) is shown in Fig. 9(a). While only minor multiple-related artefacts contaminate the migration result (red arrows in Fig. 9a), some dipping interfaces are not imaged (red box in Fig. 9a). However, most structures are properly identified. As for the first experiment, multiple-related artefacts contaminate the image if we migrate standard one-way extrapolated wavefields (red arrows in Fig. 9b). Blue arrows in Fig. 9(a) point at structures clearly visible in the Marchenko image that are partially or totally overshadowed by coherent noise in the standard one-way extrapolation result. Whereas the occurrence of only minor false positives (i.e. multiple-related artefacts) testifies the potential of the method, the presence of false negatives (i.e. the inability to image dipping interfaces) also indicates its limitations. The dipping structures in the red box are not imaged due to the poor illumination provided by horizontal areal sources. Despite this limitation, the method provides an unexpensive multiple-related free image which could be used to guide more expensive target imaging methods to areas of interests otherwise overshadowed by coherent noise in the standard one-way extrapolation results (such as that of Fig. 9b).

Moreover, we can improve the imaging results at a small cost by simply employing dipping boundaries in the subsurface and retrieving, via solution of an appropriate Marchenko equation, in- and outpropagating areal-source responses associated with tilted planes

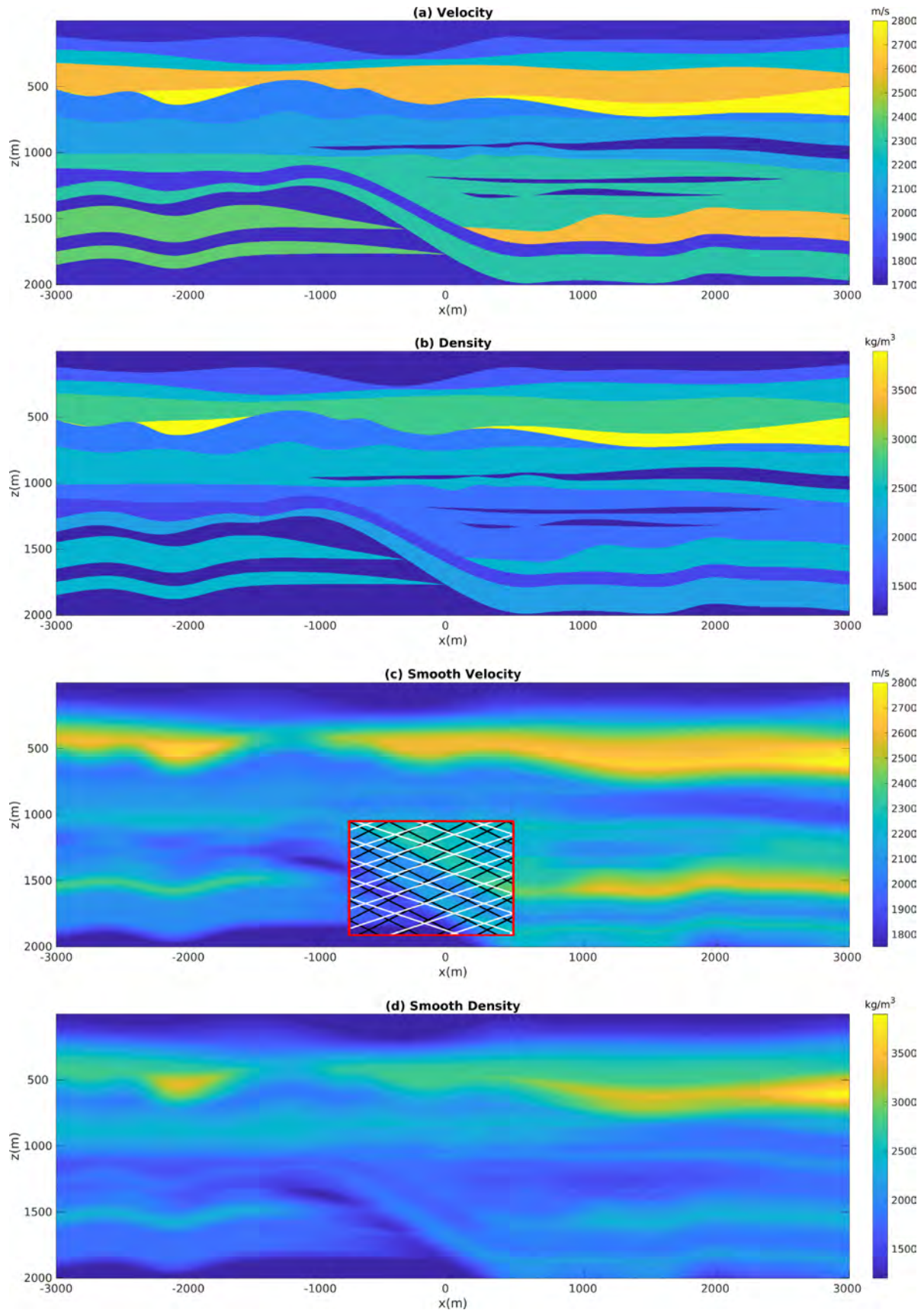


Figure 8. (a) Velocity model used in the second numerical experiment. (b) Density model used in the second numerical experiment. (c and d) Smooth velocity and density models used to provide input for Marchenko redatuming. The red box in (c) indicates a subzone of the model where tilted planes, represented by white and black lines, are used to improve the final imaging result.

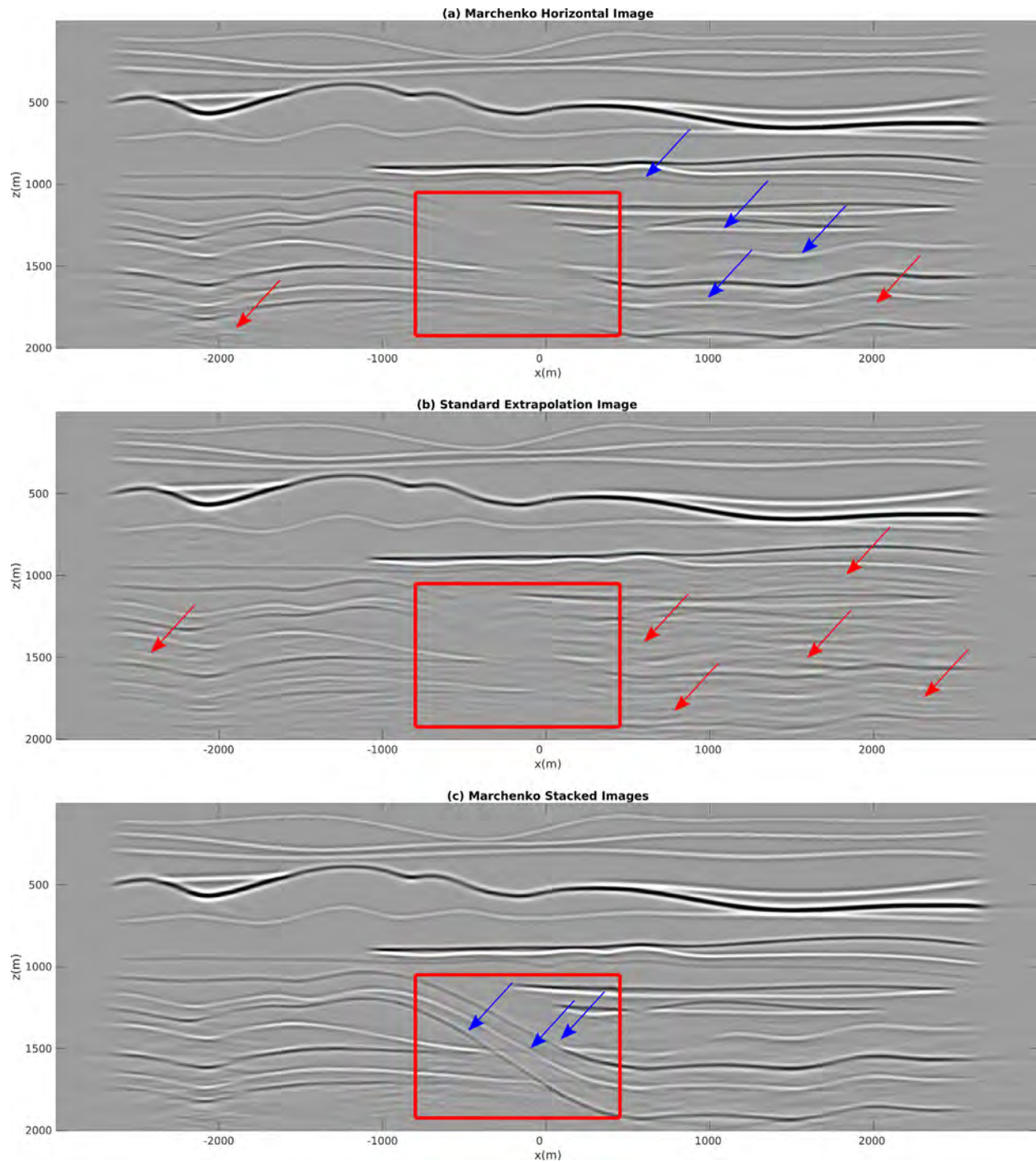


Figure 9. (a) Migration result using the imaging condition of eq. (14) and Marchenko redatumed virtual-plane wavefields. The red arrows point at low amplitude artefacts, whereas the blue arrows point at resolved structures not visible in the standard migration image. The red box encircles an area where dipping interfaces are not imaged. (b) Migration result using standard one-way extrapolation of virtual-plane wavefields. Red arrows point at multiple-related artefacts. (c) Migration result using plane-wave Marchenko wavefields associated with the tilted planes in Fig. 8(c). Blue arrows indicate dipping interfaces now properly imaged.

(the derivation of these new equations is obtained by simply replacing Λ_f in eq. 9 with a tilted boundary, and replacing downgoing and upgoing fields by outward and inward propagating fields). The retrieved wavefields provide better illumination of dipping interfaces and therefore improve the overall quality of the migration. To emphasize the benefit of this strategy, we target the area in the red box and employ four sets of dipping boundaries (white and black

lines in Fig. 8c). For the geometry considered here, 600 additional Marchenko solutions are used. The same procedure as discussed above, consisting of Marchenko areal-source response estimation and migration, is then followed. The images associated with horizontal and dipping boundary migrations are finally stacked together and the result is shown in Fig. 9(c). While no false positive is contaminating the final image, the previously invisible tilted interfaces

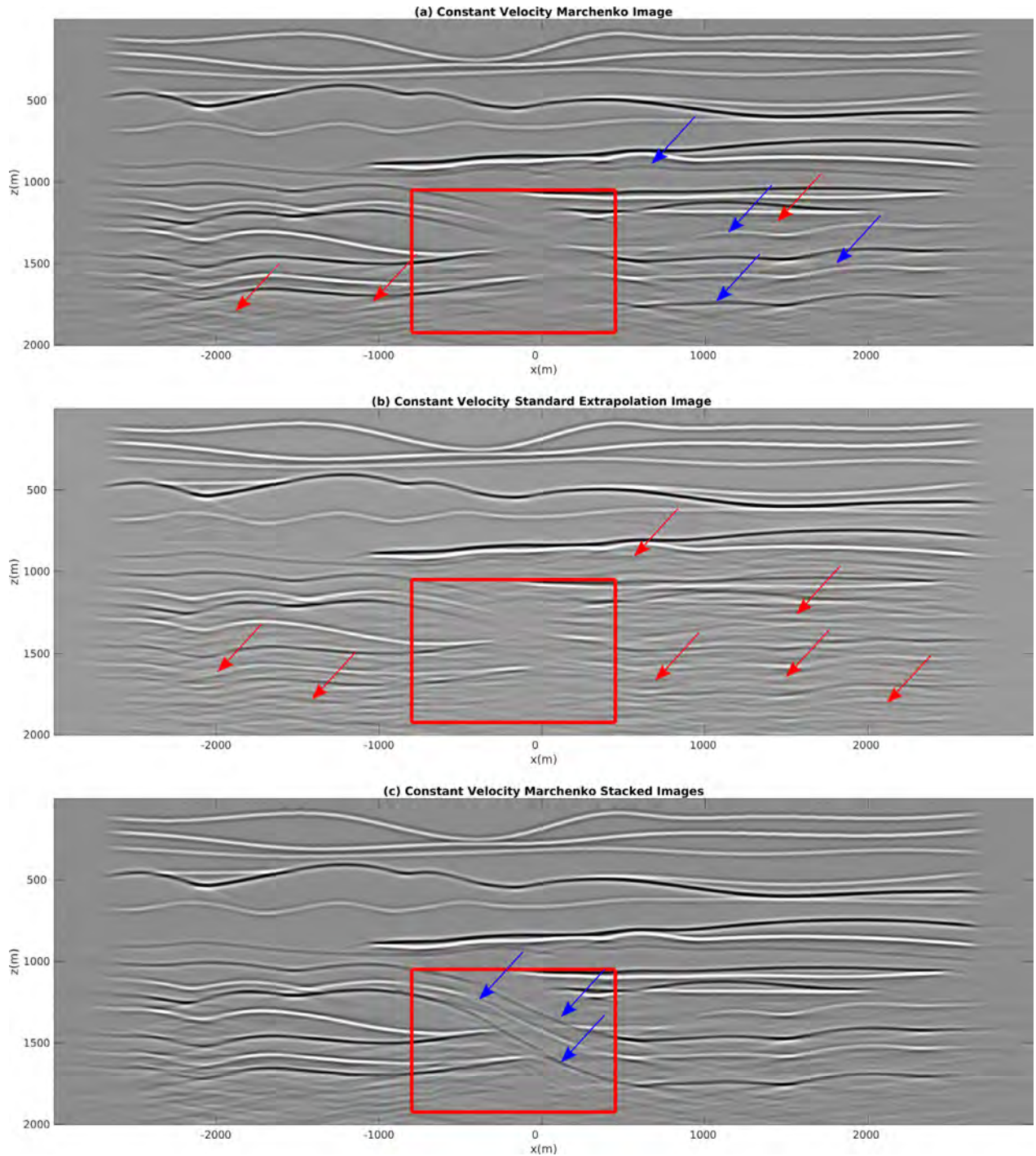


Figure 10. As for Fig. (9), but now using a simplified, constant velocity model in the redatuming and migration steps.

are now visible (blue arrows in Fig. 9c). Consider that the area of the target zone alone is about 1 km^2 , which would correspond to about 40 000 virtual source locations (at a 5 m sampling rate) if we chose to image it with other Marchenko schemes. Thus, while involving dipping boundaries increases the computation burden of the areal-source method presented here, its convenience with respect to point-source methods is still significant.

In the examples discussed above we have employed smoothed versions of the actual velocity/density models in the redatuming

and migration steps. However, in practical situations it is not always possible to have access to such good estimates of the true model parameter distributions. To assess the applicability of the method in realistic scenarios we therefore test the Marchenko areal-source scheme also assuming very poor prior knowledge of the actual velocity/density distributions. More specifically, we repeat the second experiment using homogeneous velocity/density models, setting $c = 2000 \text{ m s}^{-1}$ and $\rho = 2000 \text{ kg m}^{-3}$. Several authors have already discussed the sensitivity of the Marchenko method to various sources of errors (Thorbecke *et al.* 2013; Meles *et al.* 2015,

2016; de Ridder *et al.* 2016), and here its robustness is further tested. Fig. 10(a) shows the migration output corresponding to Marchenko horizontal areal-source responses. While the image is distorted due to the simplified velocity model employed in the migration step, only minor multiple-related artefacts contaminate the image (red arrows in Fig. 10a). This demonstrates the good performance of the plane-wave Marchenko method in suppressing standard wavefield extrapolation artefacts even if the employed velocity model is strongly simplified. On the other hand, strong multiple-related artefacts are superimposed to actual interfaces when standard one-way extrapolated wavefields are migrated (red arrows Fig. 10b). Blue arrows in Fig. 10(a) point at structures clearly visible in the Marchenko image that are partially or totally overshadowed by coherent noise in the one-way extrapolation result. As for the previous case, if we include tilted boundaries in the redatuming and migration process, the dipping interfaces are imaged (Fig. 10c).

4 CONCLUSIONS

We have demonstrated that Marchenko methods can be successfully applied beyond conventional space–time focusing. We have discussed how a modified focusing condition relates areal-source responses associated with horizontal or dipping planes to standard reflection data. A separation operator based on specifically designed direct focusing functions can then be applied to convolution/cross-correlation representation theorems to retrieve areal-source responses at the surface through standard Marchenko algorithms. The retrieved wavefields can be used to produce images, free of multiple-related artefacts, at a fraction of the cost of standard Marchenko approaches, thus potentially guiding expensive target imaging and being applicable also for 3-D data sets. While more complex problems could deteriorate the performances of the proposed method, the results discussed above demonstrate its applicability to a large class of problems. Analysis and assessment of the resolution properties of the proposed method with respect to standard Marchenko imaging and its extension to elasticity are topics of ongoing research.

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